# Dielectric, thermal and sintering behavior of BaO-B<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> glasses with the addition of  $Al<sub>2</sub>O<sub>3</sub>$

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**Abstract** In the Pb-free low temperature sinterable glass of the  $(55)BaO-(35)B<sub>2</sub>O<sub>3</sub>-(10)SiO<sub>2</sub> system, different amounts$ of  $Al_2O_3$  were added and the crystallization behavior, sintering behavior and physical characteristics of the glass were examined. It was found that  $Al_2O_3$  suppressed crystallization of the glasses because it played the role of a network former. The glass transition temperatures, crystallization temperatures, and optimum sintering temperatures increased as the amount of  $Al_2O_3$  increased. In the case of a specimen with a large amount of  $Al_2O_3$ , which was not easily crystallized, an over-firing phenomenon was observed when the sintering temperature was higher than the optimum sintering temperature. While the over-firing phenomenon was not observed due to the crystallization in the sample with a little amount of  $Al_2O_3$ . The dielectric constant and thermal expansion coefficient of the glasses were also examined and explained in correlation with the crystallization and densification.

**Keywords** Sintering . Low temperature sinterable glass . Crystallization . Over-firing . Densification

# **1 Introduction**

Significant developments in various electronic industries such as flat panel displays, low-temperature cofired ceramics, and the packaging industry need a variety of new glasses, which can be easily densified at low temperatures [1–3]. Barrier rib material in plasma display panel (PDP) is made up of glass frit-ceramic composites, and PbO containing glasses such as the PbO-B<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> and PbO-B<sub>2</sub>O<sub>3</sub>-ZnO systems have been popular as a commercial, low temperature sinterable glass [4–6]. Recent nature protection issues, however, restrict the wide use of the PbO system, so that the development of environmentally-friendly materials, which can replace the PbO, has been affected  $[7-9]$ .  $Bi<sub>2</sub>O<sub>3</sub>$ , BaO and ZnO have been employed as candidate materials that can replace PbO, particularly in the PbO-B<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> system [7–9]. In this case, in order to obtain low glass transition temperatures, unlike the PbO glass system, much amount of glass network modifier is necessary, thus resulting in glass crystallization [9, 10]. The crystallized phase obviously affects the property and sintering behavior of the glasses. For controllable crystallization, the addition of intermediate  $Al_2O_3$  could be considered [11]. When the molar ratio between the network modifier and intermediate  $Al_2O_3$  is greater than 1, that is, the excessive network modifier is contained in the glass,  $Al^{3+}$ ion coordinates with the 4 ions and acts as a network former, and the valence of  $Al^{3+}$  is compensated by the network modifier [12]. Therefore, crystallization could be suppressed in glass containing an excessive network modifier since  $Al_2O_3$ is effective as a network former.

In this study, therefore, the Pb-free  $(55)BaO-(35)B<sub>2</sub>O<sub>3</sub>$ - $(10)SiO<sub>2</sub>$  system, which easily crystallizes during sintering, was selected for the application to PDP barrier rib [13]. Different amount of  $Al_2O_3$  was added and the crystallization temperature, glass transition temperature, dielectric constant and thermal expansion coefficient of the glasses were analyzed. The sintering behavior of the glasses was also examined in correlation with crystallization behavior.

# **2 Experimental**

High purity chemicals BaCO<sub>3</sub> (99.6%),  $H_3BO_3$  (99.9%),  $SiO<sub>2</sub>$  (99.9%) and  $Al<sub>2</sub>O<sub>3</sub>$  (Kojundo chemical lab co.,

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**Fig. 1** X-ray diffraction patterns of sintered specimens with (a) 0 mol%, (b) 5 mol% and (c) 9 mol% of  $Al_2O_3$ 

Ltd, 99.9%, Japan) were used as starting raw materials. The amount of  $Al_2O_3$  in the compositional equation of (1−*x*)(55BaO-35B2O3-10SiO2)-(*x*)Al2O3 was changed where  $x = 0, 3, 5, 7, 9$  mol%. Weighed raw powder batches were mixed in an alumina crucible for 15 min and melted at  $1200\degree$ C for 30 min in a Pt crucible. The molten glass in the crucible was put into cold water for quenching. The glass frit was roughly crushed in an alumina mortar then Planetarymilled for 2 h at 400 rpm. The transition temperature of the glasses was measured by using a DSC (Thermal Analyzer, DSC 2920, TA Instruments, U.S.A).

The glass powders were cold isostatically pressed under a pressure of 100 MPa for 3 min in order to form green pellets. The pellets were sintered at 500–560◦C for 2 h with a heating rate of 5◦C/min, then they were furnace cooled. The density of the sintered pellets was measured by the Archimedes method. The crystal structure of the glass powders and sintered specimens was analyzed by using an Xray diffractometer (MO3-XHF, MAC Science Co., Japan). The thermal expansion coefficient of the sintered specimens was measured by using a dilatometer (DIL 402 C, Netzsch, Germany). Dielectric characteristics of the sintered specimens were analyzed by using an impedance gain phase analyzer (HP-4194A, USA) at 1 MHz.

## **3 Results and discussion**

X-ray diffraction patterns of sintered bodies are shown in Fig. 1, for different  $Al_2O_3$  content as a function of sintering temperature. The crystallization of the glass started at 515◦C for 0 mol%  $A1_2O_3$ , 550°C for 5 mol%  $A1_2O_3$ , and 580°C for 9%  $Al_2O_3$ . As the amount of  $Al_2O_3$  increased, the crystallization temperature increased. This suggests that  $Al_2O_3$  in the glass acts as a network former and increased the crystallization temperature. In every specimen, the  $BaB<sub>2</sub>O<sub>4</sub>$  and B2O3 phases were crystallized.



Fig. 2 The effect of the addition of  $Al_2O_3$  on crystallization temperature, optimum sintering temperature and glass transition temperature  $(^\circ C)$ 

Figure 2 shows the crystallization temperature, optimum sintering temperature, and glass transition temperature, as a function of the  $Al_2O_3$  amounts. These temperatures gradually increased as the amount of  $Al_2O_3$  increased. Note that the crystallization temperature increased more rapidly than the others. The densification behaviors of glasses with different amounts of  $A<sub>12</sub>O<sub>3</sub>$  are shown in Fig. 3. The optimum sintering temperature, at which the relative density became its highest value, was observed at a temperature 10◦C higher than the glass transition temperature, regardless of the  $Al_2O_3$ content. In the case of the sample without  $Al_2O_3$ , crystallization occurred near the optimum sintering temperature of 515◦C. However, it was observed that, with the addition of 9 mol%  $Al_2O_3$ , crystallization started at 580 $°C$ . This was almost 45◦C higher than its optimum sintering temperature of 535◦C.

Changes in the relative density of the sintered samples are shown in Fig. 3 for different  $Al_2O_3$  content as a function of the sintering temperature. Without  $Al_2O_3$ , the sample



**Fig. 3** Relative density  $(g/cm<sup>3</sup>)$  of specimen sintered at various temperatures

shows its maximum densification at 515◦C and the density became almost plateau above the temperature. With the addition of 9 mol%  $Al_2O_3$ , however, the relative density rapidly decreases with the sintering temperature above the optimum sintering temperature of 535◦C. This is the so-called overfiring phenomenon [14]. It can also be observed that the overfiring phenomenon is facilitated by increasing the amount of  $Al_2O_3$ .

Figure 4 shows the SEM images of specimens with 0 mol%, 5 mol%, and 9 mol%  $Al_2O_3$  sintered at their optimum sintering temperatures. Figure 4(a), (b), and (c) were sintered at their optimum sintering temperatures and (d), (e), and (f) were sintered at temperatures  $25^{\circ}$ C higher than the optimum sintering temperature. Without the addition of  $Al_2O_3$ , as shown in Fig. 4(a), the specimen showed the presence of a crystallized phase on the surface which was formed during sintering at its optimum sintering temperature of 515◦C. This resulted in high densification with a small amount of pores. Similar densification and crystalline phases were observed at 540◦C in Fig. 4(d). For the specimen with

the addition of 9 mol%  $Al_2O_3$ , crystallization did not occur and the smooth fracture surface, which is the typical feature of glass, was observed after sintering at its optimum sintering temperatures of  $535^{\circ}$ C and  $560^{\circ}$ C as shown in Fig. 4(c) and (f). By increasing the temperature above its optimum sintering temperature, however, this gives rise to the formation of large pores as shown in Fig. 4(f). This caused the decrease in the relative density due to the over-firing phenomenon, as shown in Fig. 3. With the addition of 5 mol%  $Al_2O_3$ , the specimen, sintered at its optimum sintering temperature of  $525^{\circ}$ C formed a smooth surface as shown in Fig. 4(b). In Fig. 4(e), however, a rough surface was observed due to the crystallization of the specimen sintered at 550◦C. It is also noted that large pores did not form at that temperature. Therefore, the increase in  $\text{Al}_2\text{O}_3$  suppresses crystallization near the optimum sintering temperature and leads to the over-firing phenomenon of specimens above the optimum sintering temperature.

A schematic diagram, explaining the relationship between over-firing and the crystalline phase, is shown in Fig. 5. When crystallization does not occur at the optimum sintering temperature, increasing the temperature above it causes the coalescence and expansion of pores that lead to the formation of large pores as illustrated in Fig. 5(a). It is generally observed that small isolated pores are generated during the sintering process of glass powders. The small pores can easily move to coalesce with adjacent pores and grow to large pores as the temperature increases because the viscosity of the glass decreases with the temperature. When pore coalescence occurs, it results in an increase in the pore radius and a decrease in pore pressure. Therefore, the volume of the pore after coalescence is larger than the sum of the pore volumes before the coalescence which led to the generation of macro pores [15]. Figure 5(c) shows a case where large pores did not form in the specimen which was crystallized near the optimum sintering temperature even after sintering above the optimum sintering temperature. Generally, the viscosity



**Fig. 4** Fracture surface photographs of samples with (a, d) 0 mol%, (b, e) 5 mol%, and (c, f) 9 mole% of  $Al_2O_3$  sintered at optimum sintering temperature and 25◦C above it



**Fig. 5** Schematic diagrams explaining pore coalescence in specimens with and without crystallized phases

of the glass increases with the addition of the crystalline solid phase [16]. In the specimens which were crystallized near the optimum sintering temperature, as in the case of the 0 mol% and 5 mol%  $Al_2O_3$  added specimens, the crystalline phase gives rise to a increase of viscosity that hinders the coalescence of the pores. As a result, the suppression of the over-firing phenomenon could be explained by this mechanism.

Figure 6 shows the thermal expansion coefficient  $(\alpha)$  and dielectric constant  $(\varepsilon_r)$  of specimens sintered at their optimum sintering temperatures. In the case of the compositions on the right hand side of the dotted line in Fig. 6, the  $\alpha$  decreased gradually from 13.4  $\times$  10<sup>-6</sup>/°C to 11.3  $\times$  10<sup>-6</sup>/°C as the  $Al_2O_3$  content increased. The  $\varepsilon_r$  also decreased from 12.6 to 12.1. It is thought that the decrease of  $\alpha$  is caused by the increase in the content of  $Al_2O_3$ , which played the role of a network former. In the case of  $\varepsilon_r$ , since Al<sub>2</sub>O<sub>3</sub> reduced the fraction of nonbridging oxygens, which have high polarity, the  $\varepsilon_r$  is thought to decrease. On the other hand, in the case of 0 mol%  $Al_2O_3$  on the left hand side of the dotted line, the  $\alpha$  was 13.42 × 10<sup>-6</sup>/°C, which is higher than the compositions on the right hand side. This seems to be attributed to the crystallization of the  $BaB<sub>2</sub>O<sub>4</sub>$  phase in the specimen. Since the BaB<sub>2</sub>O<sub>4</sub> structure has a high anisotropic  $\alpha$  of  $36 \times 10^{-6}$  c along the *c* axis, the crystallization of the  $BaB<sub>2</sub>O<sub>4</sub>$  phase obviously affects the  $\alpha$  of the specimen. The low  $\varepsilon_r$  in 0 mol%  $Al_2O_3$  is also believed to be due to the crystallization of the BaB<sub>2</sub>O<sub>4</sub> phase since the  $\varepsilon_r$  of BaB<sub>2</sub>O<sub>4</sub> is around 5–8 which is lower than the matrix.



**Fig. 6** The effect of the addition of  $Al_2O_3$  on the thermal expansion coefficient ( $\alpha$ ) and dielectric constant ( $\varepsilon_r$ )

### **4 Conclusions**

In conclusion, the effects of  $Al_2O_3$  on the sintering behavior and properties of the BaO-B<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> glass system are reported. As the amount of  $Al_2O_3$  increased, the crystallization temperature, optimum sintering temperature, and glass transition temperature increased. The addition of  $Al_2O_3$  reduced the amount of the crystalline phase so that the overfiring phenomenon occurred above the optimum sintering temperature. This suggests that the crystalline phase acts as an important role in the densification of glass. The thermal expansion coefficient decreased with the addition of  $Al_2O_3$ because it played the role of a network former and tightened the network structure. The dielectric constant also decreased with the addition of  $Al_2O_3$  due to the reduced the fraction of nonbridging oxygens.

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